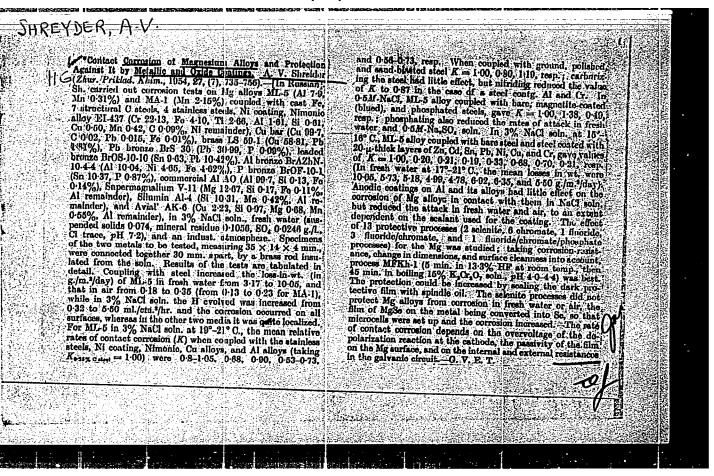
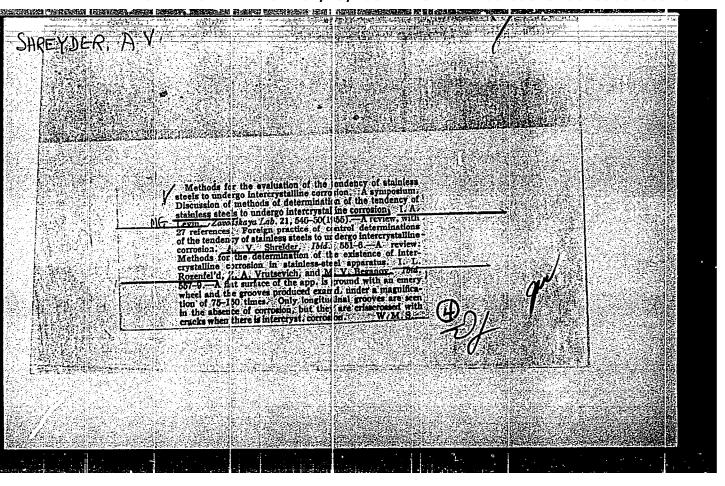
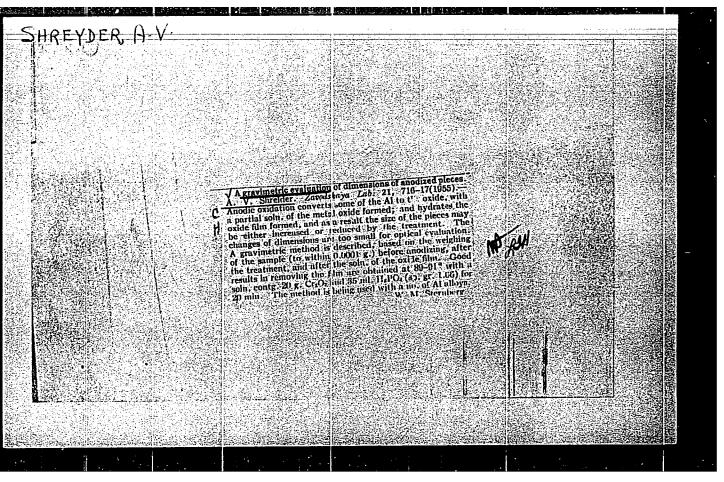
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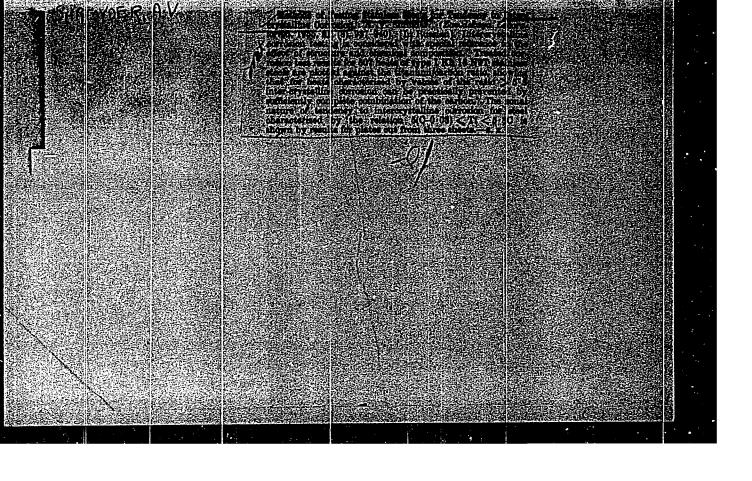




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AID P - 3492

SHREYDER A.V.

Subject

: USSR/Chemistry

Card 1/1 Pub. 152 - 7/21

Author Shreider, A. V.

Title Some characteristics of intercrystalline corrosion of

austenitic stainless steel

Periodical Zhur. prikl. khim., 28, 6, 608-615, 1955

Abstract

The zonal tendency to intercrystalline corrosion of various steels was studied. The grain size and the Ti:C ratios of the YalT steel are discussed, and a minimum Ti:C ratio of 5.8 suggested. Five diagrams,

11 references, 9 Russian (1945-1954).

Institution None :

Submitted N 9, 1953

KHALETSKIY, Nikolay Mithaylovich, inzhener; UDAL'TSOV, A.N., glavnyy redaktor; SHREYDER, A.V., kandidat tekhnicheskik nauk, redaktor

[Semiautomatic instruments for measuring the thickness of the cathodo costing on electronic instruments] Poluavtomaticheskii pribor dlia izmoreniia tolshchiny pokrytiia katodov elektronnykh priborov. Tema 9, no. P-56-430. Moskva, Akad. nauk SSSR, 1956.

9 p. (Measuring instruments)

(Measuring instruments)

AZHOGIN, Fedor Fedorovich, kend.tekhn.nauk; SHRRYDER, A.V., kend.tekhn.

neuk, red.; UDAL'TSOV, A.N., glavnyy red.

[Local oxidation of magnisium alloys] Mestnoe oksidirovanie

megnievykh splavov. Moskva, In-t tekhniko-ekon.inform.. 1956. 13 p.

(Informatsiie o nauchno-iseledovetel'skikh rebotskh. Tema 23.

no.I-56-11)

(Magnesium alloys) (Oxidation)

GAKMAN, Emma Livovna; RAGAZIMA, M.F., inzhener, vedushchiy redaktor; SHREYDER, Aukor kandidat tekhnicheskikh nauk, redaktor; PONCKAREV, V.A., tekhnicheskiy redaktor

[Zinc plating of parts] Diffuzionnoe tsinkovanie detalei. Moskva. Akad.nauk SUSR, 1956. 15 p. (Informatsiia o nauchno-issledovatel'-skikh rabotakh. Tema 24, no.I-56-207) (MIRA 10:10) (Zinc plating)

SHREYDUR. Aleksandr Viktorovich, kani.tekhn.nauk; UDAL'TSOV, A.N., glavnyy red.; ZARETSKIY, Ye.M., kand.tekhn.nauk, red.

[Controlling corrosive disintegration of brass pipes] Bor'ba korrozionnym rastreskivaniem latunnykh truboprovodov. Moskva, In-t tekhniko-ekon. inform., 1956. 19 p. (Informatsiia o nauchnoissledovatel'skikh rabotakh. Tema 23, no.I-56-5) (MIRA 11:2) (Brass--Corrosion) (Pipe)

KOSHELEV, Grigoriy Grigor'yevich; KIARK, Gel'ma Brunovna; UDAL'TSOV, A.N., glavnyy red.; SHREYDER, A.V., kand.tekhn.nauk, red.

[Practices of protecting marine installations of the petroleum industry from corrosion by means of protective devices] Opyt zashchity morskikh neftepromyslovykh sooruzhenii ot korrosii s pomoshch'iu protektorov. Moskva, In-t tekhnikoOekon.inform.. 1956. 21 p. (Informatsiis o nauchno-issledovatel'skikh rabotakh. Tema 23, no.I-56-140) (MIRA 11:2)

(Corrosion and anticorrosives)
(Petroleum industry--Equipment and supplies)

SHKEY DER, A.V.

BOBYLEV, Aleksey Vasil'yevich; TOMASHOV, N.D., professor doktor, retsensent; TURKOVSKAYA, A.V., kandidat tekhnicheskikh nauk; SHREYDER, A.V., redaktor; ARKHANGEL'SKAYA, M.S., redaktor; MIKHAYLOVA, V.V., tekhnicheskiy redaktor.

[Disintegration of brass caused by corrosion] Korrosionnoe rastreskivanie latuni. Moskva. Gos.nauchno-tekhn. izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1956. 120 p. (MLRA 9:5)

(Brass--Corrosion)

### "APPROVED FOR RELEASE: 07/13/2001 C

CIA-RDP86-00513R001550010004-5

SOV/137-57-6-10856

Translation from: Referativnyy zhurnal, Metallurgiya, 1957, Nr 6, p 207 (USSR)

AUTHOR: Shreyder, A.V.

TITLE: Erosive Wear of Metals and Protection by Coatings (Erozionnyy

iznos metallov i zashchita pokrytiyami)

PERIODICAL. V sb.: Povysheniye iznosostoykosti i sroka sluzhby mashin.

Kiyev-Moscow, Mashgiz, 1956, pp 368-375

ABSTRACT: An examination is made of abrasive, erosive wear occurring when artificial gas flows are transmitted over metal surfaces at high velocities. Evaluation of the erosion life (EL) of materials is made on an instrument specially designed for the purpose (a schematic diagram

of the instrument is presented). The major experiments are run under sand blast at 275 m/sec. The specimen is subjected to erosion at an angle of 45° at a nozzle distance of 180 mm. Weight-loss measurement is the method used to evaluate EL in hard metals and coatings, while for soft metals, in view of the fact that the sand particles are found to wedge into the surface layer, depth of destruction is

measured by means of a thread micrometer with a sharp-tipped in-

Card 1/2 sert. The EL of Nr 20 steel is used as the standard of comparison.

SOV/137-57-6-10856

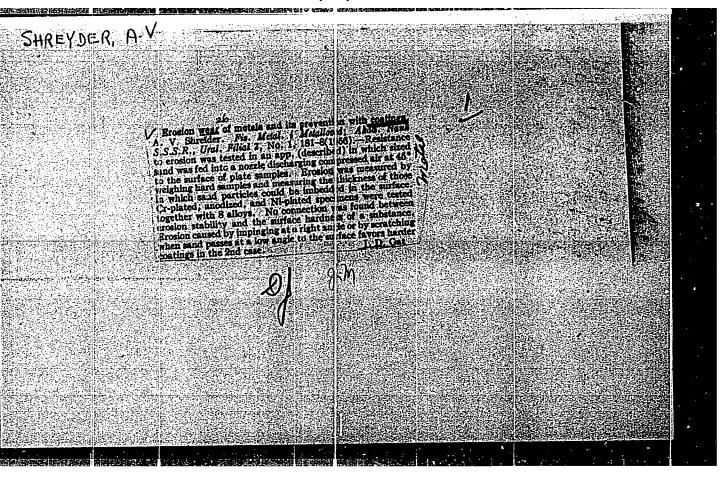
Erosive Wear of Metals and Protection by Coatings

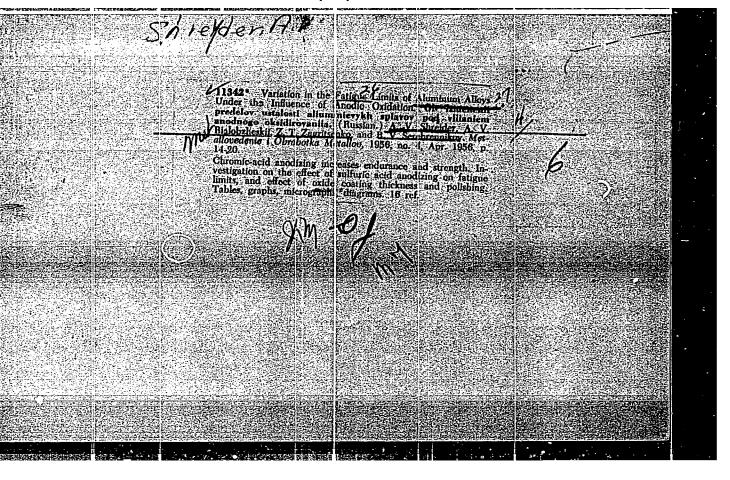
HERRICHER HELEN DESCRIPTION OF THE PROPERTY OF THE PROPERTY OF THE PARTY OF THE PAR

The erosion-protective properties of thin anode-oxide films are evaluated interms of the time required for the oxide to be worn away. It is shown that the EL of materials cannot be established by determinations of hardness to indentation or scratch hardness, or by determination of resistance to frictional wear. This is explained by the fundamental differences between the mechanism of erosion and that of abrasion, deformation, and failure upon frictional wear and the impressing of an indenter. It is found that ordinary mild steel has greater EL than EYalT steel or Cu, Al, and Mg alloys. A significant increase in the EL of ferrous and nonferrous metals is attained by hard chromium plating and in that of Al alloys by thick anodizing. A study is made of the influence of the angle of impingement, the impact speed of the particles, the duration of erosive action, and the roughness of the metal surface upon erosive wear, and the mechanism of erosive destruction of hard and ductile metals is described. The proposed method of investigating the EL of materials makes it possible to arrive at an empirical determination of the relationship between erosive destruction and the factors indicated above, and to determine the relative EL of oxides produced by anodizing Al alloys in various ways. See RZhMet, 1957, Nr 1, abstract 1121.

L.G.

Card 2/2

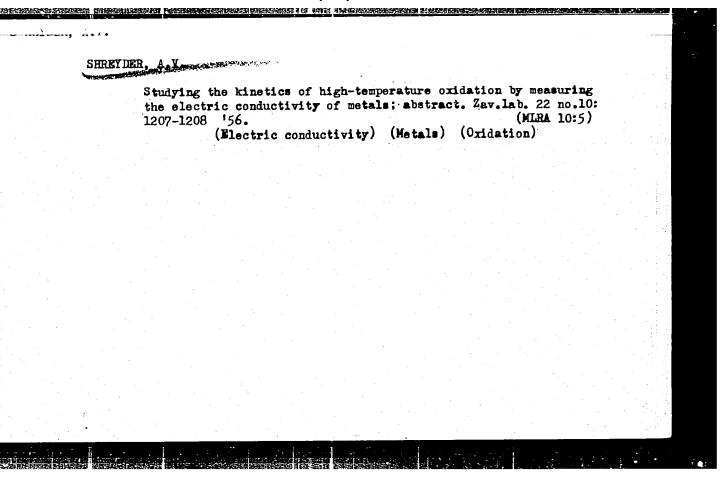


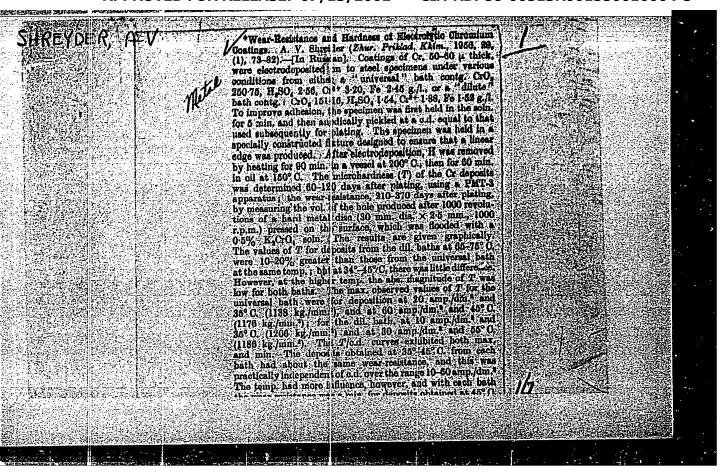


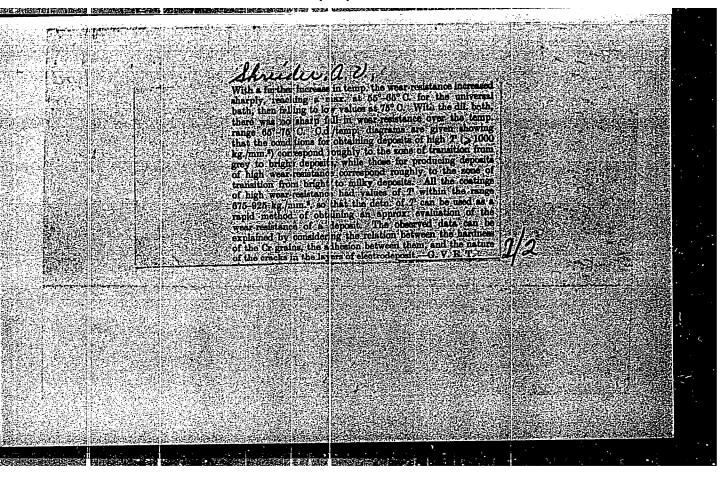
FIGEL'MAN, M.A.; SHREYDER, A.V.

Investigation of hydrogen embrittlement of steel. Zav.lab. 22 no.5: 586-588 '56. (MIRA 9:8)

(Steel--Brittleness)







USSR/Corrosion - Protection From Corrosion

J.

Abs Jour

: Referat Zhur - Khimiya, No 4, 1957, 14101

Author

: Shreyder A.V.

Title

: Control of Corrosion Fissuration of Brass Collectors

of Liquid Fuel

Orig Pub

: Zh. prikl. khimii, 1956, 29, No 7, 1044-1056

Abstract

Investigation of corrosion fissuration (CF) of brass dollectors of liquid fuel, operating under pressure, has shown that this damage is due not to action of fuel, containing up to 0.13% sulfide S, but due to the action of air contaminated with ammonia. Protection against CF of brass (B) in copper-ammonia media by cadmium plating effected by a shift of the potential of B in the negative direction; as a result thereof a decrease occurs in the tendency to adsorptive lowering of strength as well as to a dissolution of B at the areas devoid of the donting. Comparison of resistance to CF of brass 68 and

Card 1/2

-9-

SHARYDER, AN.		
	Levin, A. I	
	25(0) PHASE I BOOK EXPLOITATION SON/1940	
	Akademiya menk SSSM. Institut fizicheskoy khinti	
	Teoriya i praktika elaktroliticheskogo khrumirovaniya (Theory and Fractice of Electrolytic Chromium Flating) Moscow, Ind-vo AM SSSR, 1957. 231 p. 5,000 copies printed.	
	Resp. Eds.: Vagranyan, A.T., Professor, H.T. Khiryavisev, Professor, and H.A. Shluger, Candidate of Technical Sciences; Ed. of Publishing House: Tegorov, B.G.: Tech. Ed.: Pavlovskiy, A.A.	
	FRENCES: This book is for engineers, industrial workers, numbers of accentific research institutions and teachers concerned with modern methods of electroplating and the meanfacture of corrosion—resistance.	
	CONTRACE: The epilection contains sixteen reports and the texts of several discussions presented before the March 1955 Conference on the Theory and Fractice of Chronium Flaths, sponsored Mainly W the Lastitute of Physical Chemistry, 81 USES, and the Moscow Scientific, Segmenting and Technical Society for Instrument Mainles. The reports reflect the conference's aim of a wide unchange of opinion on problems of champium electrodeposition and offer scalations.	
	and the solutions	
	Entroise A. V. The Influence of Electrodeposition Farameters on the  Hardwood Man Pear-resistance of Chromium Findings	
	TI	

SOV/137-58-7-15452

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 7, p 218 (USSR)

AUTHOR: Shreyder, A.V.

Influence of the Parameters of Electrolytic Deposition on the TITLE:

Hardness and Wear Resistance of Chrome Coatings (Vliyaniye parametrov elektroosazhdeniya na tverdost' i iznosostoykost'

khromovykh pokrytiy)

V sb.: Teoriya i praktika elektrolit. khromirovaniya. Moscow, PERIODICAL:

AN SSSR, 1957, pp 77-96

The influence of the method of chrome plating on the microhardness (M) and wear resistance (W) of a chrome coating (CC) ABSTRACT:

was studied. Chrome plating was carried out in a universal electrolyte (in g/1: CrO<sub>3</sub> 250.75, H<sub>2</sub>SO<sub>4</sub> 2.56, Cr<sup>3+</sup> 8.20, Fe 2.45) and a diluted electrolyte (in g/l: CrO3 151.16, H2SO4 1.54, Cr3 + 1.88, Fe 1.52) at different temperatures (35-75°C) and cathode cd's (10-110 amp.dm<sup>2</sup>). The thickness of the CC was 50-60  $\mu$  . Before plating the surface of the specimen to be plated was polished and degreased with B-70 benzene. To ensure a strong bond between CC and the specimen, the latter

was kept in the electrolyte for 5 minutes with subsequent anodic

Card 1/3

SOV/137-58-7-15452

Influence of the Parameters of Electrolytic Deposition (cont.)

pickling. Elimination of the phenomenon of "tracing" of lines by the ribs of the specimen was achieved by specially constructed devices. A description and drawing of the devices are given. For the removal of H2 the specimen was held for 1 hr 30 min at 2000 and 1 hr in oil at 1500. Measurement of M was performed by the PMT-3 apparatus during an interval of 60-120 days after chrome plating with a load of 100 g. W was determined by abrasion of the specimen with a polishing disk of a superhard alloy with a sliding speed of 1.6 m/sec wetted with a 0.5% water solution of K2CrO4, and the size of resulting pitting on the surface (measurement was made under a microscope). The reciprocal of the volume of the pitting craters (mm<sup>-3</sup>) multiplied by 1000 was taken as a criterion of W. W was determined in the interval between 210-370 days from the time of chrome plating. The test error amounted to 8-10%. M and W were determined for CC produced in either electrolyte in the range of cathode cd and temperature most generally used in practice. A high W is produced with M equal to 650-925 kg/mm<sup>2</sup>, with which the strength of the grains of Cr does not surpass the strength of their mutual bond. With high M values, when the strength of the grains of Cr exceeds the strength of their mutual bond, W decreases because of the crumbling of the grains. Chrome-plating procedures (cathode cd and temperature) in either electrolyte is proposed for production of CC with a high Card 2/3

SOV/137-58-7-15452

Influence of the Parameters of Electrolytic Deposition (cont.)

( $\geq$ 1000 kg/mm<sup>2</sup>) M and W ( $\geq$ 50 mm<sup>-3</sup>). It is indicated that M may be used as a quick method for the determination of W of electrolytic CC. Bibliography: 20 references.

T.M.

1. Chromium plating--Mechanical properties 2. Surfaces--Preparation

Card 3/3

# SHREYDER, A.V., referent.

Electrochemical method for determining the anticorrosive properties of bituminous insulation of underground pipelines. Zav. lab. 23 no.3:339 '57. (MIRA 10:6)

'57.
(Electrolytic corrosion and anticorrosives)
(Bituminous materials)

KETUIF, NIF

AUTHOR:

Shreyder, A.V., Reviewer

**公共等於其一個公司的內部的公司的日本公司的公司的 第二日第二年第** 

32-12-31/71

TITLE:

A Method of Determining the Corrosion-Resisting Quality in the Diffusion of Hydrogen Through the Walls of a Hermetically Closed Hollow Sample, Which is Filled With the Corrosion Medium (Abstract) (Metodika otsenki korrozionmoy stoykosti po diffuzii vodoroda cherez stenki germetizirovannogo pologo obraztsa, zapolnyayemogo korrozionnoy sredoy) (Referat).

PERICDICAL:

Zavodskaya Laboratoriya, 1957, Vol. 23, Nr 12, pp. 1471-1471 (USSR)

ABSTRACT:

This is an abstract of the paper by Bloom et al., which was published in "Corrosion" (1957), 13, Nr 5, pp. 27-32. The method concerned had been adapted to the operational conditions of nuclear reactors and serves the purpose of determining the corrosion properties of metals under the action of hydrogen depolarization in cathode processes. For the experiment a piece of steel tube was filled with the corrosion liquid (a solution of lye and water). Its ends are bent in and welded. The sample obtained in this manner (capsule) was connected with a ferromagnet as a counterweight and by means of a pulley block it was conveyed into a system of quartz tubes and closed. That part of the system which contains the sample was heated

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A Method of Determining the Corrosion-Resisting Quality in the Diffusion of Hydrogen Through the Walls of a Hermetically Closed Hollow Sample, Which is Filled With the Corrosion Medium

32-12-31/71

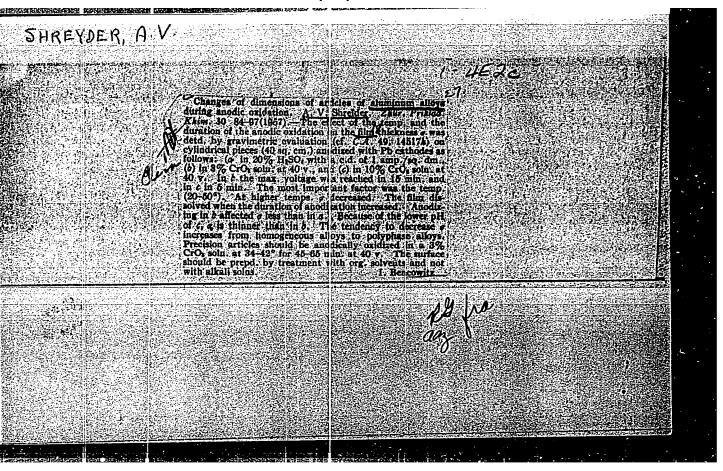
up to 315°. As a result of the heating of the sample its walls became corroded. The hydrogen separated by depolarization and diffused through the walls of the sample increased the pressure in the closed system, which was recorded by the automatic pressure gauge provided. It was found that by the admixture of lye to the corrosion liquid hydrogen diffusion is diminished because a protective crust forms on the inside part of the walls of the sample (tube capsule). As soon as cracks occur in the crust as a result of thermal action (extension of the sample) pressure increases; it is reduced again as soon as a new crust is formed. There is 1 figure and 1 Slavic reference.

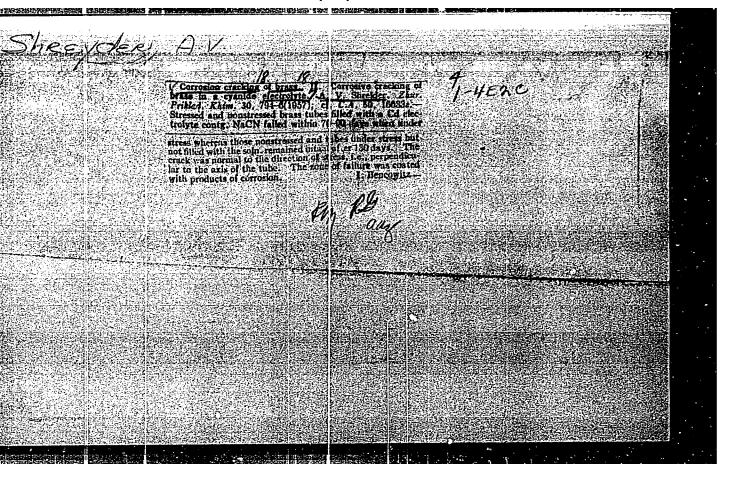
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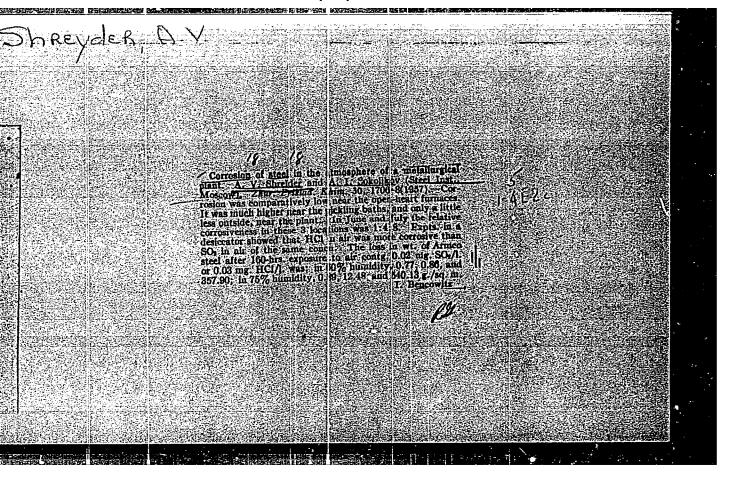
Library of Congress

Card 2/2

 Hermetically sealed samples-Hydrogen resistance-Corrosion resistance-Determination







FIGEL'MAN, M.A.; SHREYDER, A.V.

Hydrogen brittleness of steel in cathode processing. Zhur. prikl.

khim. 31 no.8:1184-1193 Ag '58.

(Steel--Brittleness)

SHREYDER, A.V.: ARAKELOV, A.G.

Mechanism of alkaline oxidation of steel. Zhur.prikl,khim. 31
no.11:1673-1678 N '58. (MIRA 12:2)
(Steel--Corrosion)

KOROVIN, Yuriy Mikhaylovich; ULANOVSKIY, Iosif Borisovich; SHOBIK, L.Ye., inzh., ved. red.; SHREYDER, A.V., kand. tekhn. nauk, red.; SOROKINA, T.M., tekhn. red.

RESERVED THE REPORT OF THE PROPERTY OF THE PRO

[Corrosion of stainless steels in the spots in contact with non-metallic materials]Korrosiia nerzhaveiushchikh stalei v mestakh kontakta s nemetallicheskimi telami. Moskva, Filial Vses. in-ta nauchn. i tekhn. informatsii, 1958. 12 p. (Peredovoi nauchno-tekhnicheskii i proizvodstvennyi opyt. Tema 13. No.M-58-139/16) (MIRA 16:2) (Steel, Stainlesse-Corrosion)

LAYNER, Vladimir Il'ich, prof., doktor; SHREYDER, A.V., kand.tekhn.nauk, retsenzent, red.; STOKLITSKIY, L.I., inzh., retsenzent; ARKHANGEL'SKAYA, M.S., red.izd-va; DOBUZHINSKAYA, L.V., tekhn.red.

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[Electroplating of light alloys] Gal'vanicheskie pokrytiia legkikh splavov. Moskva, Gos.nauchno-tekhn.izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1959. 137 p. (MIRA 12:5) (Electroplating) (Alloys)

SHREYDER A.V.

TOMASHOV, Nikon Danilovich. Prinimali uchastiye: TYUKINA, M.N.; PALEOLOG, Ye.N.; CHERNOVA, G.P.; MIEHAYLOVSKIY, Yu.N.; LUNEV, A.F.; TIMO-NOVA, M.A.; MODESTOVA, V.N.; MATVEYEVA, T.V.; BYALOBZHESKIY, A.V.; ZHUK, N.P.; SHREYDER, A.V.; TITOV, V.A.; VEDENEYEVA, M.A.; LOKO-TILOV, A.A.; BERUKSHTIS, G.K.; DERYAGINA, O.G.; FEDOTOVA, A.Z.; FOKIN, M.N.; MIROLYUBOV, Ye.N.; ISAYEV, N.I.; AL'TOVSKIY, R.M.; SHCHIGOLEV, P.V., YEGOROV, N.G., red.izd-va; KUZ'MIN, I.F., tekhn.red.

[Theory of the corrosion and the protection of metals] Teoriia korrozii i zashchity metallov. Moskva, Izd-vo Akad.nauk SSSR, 1959. 591 p. (MIRA 13:1) (Corrosion and anticorrosives)

25(1)

PHASE I BOOK EXPLOITATION

SOV/3161

- Nauchno-tekhnicheskoye obshchestvo mashinostroitel'noy promyshlennosti, Kiyevskoye oblastnoye pravleniye
- Zashchitno-dekorativnyye i spetsial'nyye pokrytiya metallov (Protective, Decorative, and Special Coatings for Metals) Kiyev, Mashgiz, 1959. 291 p. 4,200 copies printed.
- Editorial Board: P. K. Lavorko, N. I. Litvak, and A. P. Eychis (Resp. Ed.); Ed. of Publishing House: M. S. Soroka; Chief Ed. (Southern Division, Mashgiz): V. K. Serdyuk, Engineer.
- PURPOSE: This book is intended for technical personnel in the field of protective coatings for metils.
- COVERACE: The papers in this collection, presented at a conference of the NTO Mashprom held in Odessa, deal with the mechanization and acceleration of metal-coating and plating processes performed by spraying, electrolytic, and other methods. Quality control of protective coatings is also discussed. No personalities are mentioned. References follow several of the papers.

**Card** 1/7

28(5) AUTHORS:

Gintsberg, S. A., Shreyder, A. V.

sov/32-25-6-33/53

TITLE:

On the Constant Moisture in Corrosion Chambers Operating With a Temperature Cycle (O postoyannoy vlazhnosti v korrozionnykh

kamerakh, rabotayushchikh s temperaturnym tsiklom)

PERIODICAL:

Zavodskaya Laboratoriya, 1959, Vol 25, Nr 6, p 741 (USSR)

ABSTRACT:

Accelerated corrosion tests which are intended to imitate the conditions of a tropical atmosphere require a steam pressure changing with temperature as little as possible. Saturated salt- and sulfuric acid solutions are not suited for this purpose as the steam pressure varies considerably with temperature. The use of glycerin - water mixtures is recommended.

as in this case only slight variations of steam pressure with temperature are to be observed which secures a considerable improvement with respect to the reproducibility of the test results. The solutions are not agressive and the relative moisture changes in proportion to the glycerin concentration of the solution (figure, dependence of the relative moisture of the air over glycerin solutions on the molar concentrations

Card 1/2

On the Constant Moisture in Corrosion Chambers Operating SOV/32-25-6-33/53 With a Temperature Cycle

of glycerin at 20±1°). There are 1 figure and 3 references, 2 of which are Soviet.

ASSOCIATION: Vserossiyskiy nauchno-issledovatel'skiy khimicheskiy institut promyshlennosti mestnogo podchineniya (All-Russian Scientific Chemical Research Institute of the Industry of Local

Subordination)

Card 2/2

PHASE I BOOK EXPLOITATION SOV/4623

Shreyder, Aleksandr Viktorovich, Docent, Candidate of Technical Sciences

DESCRIPTION OF THE PROPERTY OF

Oksidirovaniye alyuminiya i yego splavov (Oxidation of Aluminum and Its Alloys) Moscow, Metallurgizdat, 1960. 220 p. Errata slip inserted. 3,650 copies printed.

Reviewers: V.I. Layner, Professor, Doctor of Technical Sciences, and Ye.M. Zaretskiy, Candidate of Technical Sciences; Ed. of Publishing House: M.S. Arkhangel'skaya; Tech. Ed.: P.G. Islent'yeva.

PURPOSE: This book is intended for engineers and scientists interested in metal physics and the protection of metals against corrosion. It may also be used by teachers and students in schools of higher education.

COVERAGE: The book contains data from current Soviet and non-Soviet literature on the technology of imparting oxide coatings to aluminum alloys, and offers theoretical explanations for the mechanisms of oxidation processes as related to the chemical composition and properties of alloys. The properties of oxide films and ways of improving the corrosion resistance and physicomechanical

card 1/6

sov/4623 Oxidation of Aluminum and Its Alloys properties of metals by oxidation are also discussed. The author thanks S.A. Gintsberg, Candidate of Technical Sciences, and Engineer A.F. Ivanov for technical advice on anodizing; and N.I. Kubasova, N.A. Poletkina, Ye. V. Artamonova, and A.N. Kulikova for assisting in laboratory and plant experiments. There are 309 references: 160 Soviet, 70 English, 60 German and 19 French. TABLE OF CONTENIS: 5 Introduction Ch. I. Some Peculiarities of Aluminum and Its Alloys Ch. II. Preparation of the Surface of Aluminum and Its Alloys Before 14 Oxidation 16 A. Preliminary treatment Cleaning. surface conditioning, grinding, shot blasting, pickling, and alkaline cleaning, 19 B. Fundamental treatment Sandblasting, scratch brushing, decorative pickling, abrasive polishing in drums, polishing Card 2/6

CALCULAR CONTROL OF CO

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Card 2/3

S/184/60/000/004/007/021 A109/A029

Investigation of Corrosion Resistance of Metals in Solutions of Sulfuric and Phosphoric Acids at High Temperatures

pyrex glass and ampoules placed in an autoclave of 1Kh18N9T steel. Temeperatures varied from 250 - 300°C and the heating time form 24 - 1,501 h. Complications arose during tests of materials with low corrosion resistance as nascent hydrogen caused inner pressure, occasionally resulting in bursting of the ampoule. A detailed description of the test methods and conditions is given. The corrosion depth in mm/year after a 72-h test demonstrates clearly the effect of temperature on the corrosion of alloys. The 72-h corrosion depth logarithm depends on the reciprocal value of the absolute temperature. At corrosion in 10%-H3PO4 the phosphate layers observed on the surface of EI461 and EI629 alloys had a decisive protective character. Corrosion tests in sulfuric and phosphoric acids established a high resistance of platinum and an adequate resistance of tantalum. Niobium and its binary alloys with tantalum retain their resistance only in sulfuric acid. A low-resistance protective layer is formed on the surface of acidproof austenitic nickel-chromium-molybdenum steel and nickel-based EI461 alloy in phosphoric acid at high temperatures. Protective coatings are formed on the surface of niobium and niobium-tantalum alloys in sulfuric and phosphoroc acids. Their presence on nicbium-tantalum alloys in phosphoric acid prevents the solu-

s/081/62/000/002/054/107 B145/B101

AUTHORS:

Gintsberg, S. A., Shreyder, A. V.

TITLE:

Methods of protecting products with ferrous and non-ferrous metal joints from atmospheric corrosion with the aid of in-

PERIODICAL:

Referativnyy zhurnal. Khimiya, no. 2, 1962, 232, abstract 21216 (Tr. Vseros. n.-i khim. in-ta mestn. prom-sti, no. 9,

TEXT: Various inhibitors of atmospheric corrosion in the conservation of products with steel, brass, Zn and Ni joints are described. The following corrosion inhibitors were used: salts of mineral and organic acids with organic and mineral cations, organic and mineral acid esters, amines,  $N_2$  - heterocycles and thiocompounds. The synthesis of compounds described and not described in publications is given: cyclohexyl ammonium chromete, dicyclohexyl ammonium chromate, triethanolamine tetraborate, triethanol-Ammonium benzoate, cyclohexyl ammonium chromate, dicycloamine molybdate. Card 1/2

s/081/61/000/022/042/076 B102/B101 Investigation of the hydrogen embrittlement of steel in 18.8300 Shreyder, Referativnyy zhurnal. Khimiya, no. 22, 1961, 293 - 294, khimiya, no. 22, 1961, 293 - 294, in-ta prom-sti abstract 22K145 (Tr. Vseros. n-i. khim. as) AUTHORS: electroplating mestn. podchineniya, no. 10, 1960, 33 - 85) TITLE: TEXT: The influence of cathodic polarization conditions in acid and TEAT: The inituence of cathodic potarization conditions in acid and steel is alkaline solutions on the hydrogen embrittlement (HE) of carbon steel is alkaline solutions on the hydrogen adecration and the HE of steel we are interested out. alkaline solutions on the hydrogen embrittlement (HE) of carbon steel were pointed out. The kinetics of hydrogen adsorption and the HE of steel were stimulating action of cyanides and sulfides on hydrogen PERIODICAL: pointed out. The kinetics of nydrogen adsorption and the nE of steel studied. The stimulating action of cyanides and sulfides on hydrogen studied. The stimulating action of steel in alkaling colutions was adsorption in cathodic polarization of steel in alkaling colutions was adsorption in cathodic polarization of steel in alkaline solutions was verified. Reduction of hydrogenation in cathodic polarization of athodic treatment of temperature of adsorption in catnodic polarization of steel in alkaline solutions was verified. Reduction of hydrogenation in cathodic treatment of tempered verified. Reduction of hydrogenation in adding cro to the electrolyte metal in acid media is achieved by adding cro to the electrolyte. verified. Reduction of nydrogenation in cathodic treatment of temporal to the electrolyte. metal in acid media is achieved by adding CrO 3 Additions to alkaline electrolytes do not reduce HE considerably. The Additions to alkaline electrolytes do not reduce HE considerably. The strongest tendency to HE displays cold-deformed steel without subsequent strongest tendency to HE displays cold-deformed of the motol strong on the credominant influence of the motol strong of the motol encency to the credominant influence of the metal stress on This proves the predominant influence of the metal stress on annealing. Card 1/4

31561 S/081/61/000/022/042/076 B102/B101

Investigation of the hydrogen...

Card 2/4

the amount of HE. The increase in brittleness in electroplating is due to the presence of internal stresses in the deposits and to the hydrogen adsorption of the steel backing. The deposition of thin layers is accompanied by an increase in brittleness exceeding that of thick ones. The increase in brittleness is reduced with increasing thickness of the deposit. An intensification of the electrodeposition process may, on one hand, intensify the increase in brittleness due to decrease in current yield when the plating process is accelerated, and on the other - reduce the growth in brittleness due to a more rapid formation of deposit, serving as a barrier for the hydrogen penetration into the metal. Plating in cyanide electrolytes (zinc, cadmium, copper plating) is accompanied by considerably higher hydrogen adsorption than in acid ones. In acid baths the current yield is increased and cyanides intensifying hydrogen adsorption are absent. Nickel-plating leads to an increase in brittleness of tempered metal stronger than that of quenched metal. This is due to the predominant influence of stresses in the deposit. Any changes in chromium plating method, thickness of Cr deposit, dechroming conditions (anodic etching of chromium), interruptions of the current in chrome-plating have different effects on the brittleness of quenched and tempered steels. In

 s/081/61/000/022/042/076 B102/B101

Investigation of the hydrogen...

chrome-plating of tempered steels this is explained by a connection between increase in brittleness and the presence of internal stresses in the deposit - and for quenched steels it is assumed to be mainly due to hydrogenation of the backing. Electroplating results in a decrease of the fatigue limit, especially for quenched steel coated with nickel, then with chromium, zinc, and copper. The main effect on the recovery of plastic properties of steel after cathodic degreasing displays the temperature of the liquid medium in which dehydrogenation takes place; the effect of anodic aging is negligible. Electrolytic degreasing and dipping change the brittleness of steel in different directions which arises in subsequent metalplating in dependence on various factors, among which the structure of the basic metal is the most important one. Also shape and thickness of metal coatings and the conditions of electrodeposition have an influence: thin Cu and Ni backings reduce the brittleness arising in subsequent chrome-plating; thick Cu backings may intensify brittleness. Addition of oxidizers (CrO3, KMnO4) to acid solutions is little effective with respect to a decrease in brittleness in electrolytic cathodic treatment of quenched metal, but reduces the increase in brittleness in etching (dip) without current. Increase of Card 3/4

Investigation of the hydrogen ...

31561 S/081/61/000/022/042/076 B102/B101

current yield, current reversal, and stirring do not reduce the brittleness of quenched steel, but reduce that of tempered steel. Aging restores the plastic properties only of parts which were subjected to cathodic treatment without galvanic deposition; after polarization in alkali, plasticity is restored more rapidly and more completely in aging than after polarization in acids. Aging of steel parts with deposits may also lead to an increase in brittleness. [Abstracter's note: Complete translation.]

Card 4/4

#### "APPROVED FOR RELEASE: 07/13/2001

CIA-RDP86-00513R001550010004-5

S/080/60/033/007/014/020 A003/A001

AUTHORS:

Shreyder, A. V.

TITLE:

Amine Chromates and Esters of the Chromic Acid as Inhibitors of

Atmospheric Corrosion

PERIODICAL:

Zhurnal prikladnoy khimii, 1960, Vol. 33, No. 7, pp. 1594-1599

TEXT: Dicyclohexylammonium nitrite, cyclohexylammonium carbonate. monoethanolamine carbonate and benzoate are inhibitors of atmospheric corrosion used on a broad scale. A drawback of these inhibitors is their aggressiveness in relation to non-ferrous metals, especially zinc and copper alloys. Easily available esters of the chromic acid and also amine chromates were investigated as corrosion inhibitors. The effect of the chromates was investigated in a corrosion chamber with cyclic temperature drop at a relative humidity of 96-98% and a SO<sub>2</sub> concentration of 0.01 mg/l. The temperature cycle consisted in a 15-min heating to 40°C, holding the sample for 45 min at this temperature, cooling and holding for 2 hours at room temperature. The samples tested were made of  $y_{12}$  (U12) steel (1.2% C),  $\sqrt{1-70}$  (L-70) brass (70% Cu, 30% Zn) without coatings and steel samples with poreless zinc and nickel coatings. Samples of

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#### "APPROVED FOR RELEASE: 07/13/2001

CIA-RDP86-00513R001550010004-5

S/080/60/033/007/014/020 A003/A001

Amine Chromates and Esters of the Chromic Acid as Inhibitors of Atmospheric Corrosion

oxidized MA-2 magnesium alloy and non-oxidized A -16 (D-16) Duraluminum were also tested. The inhibitors were introduced into wrapping paper in the amount of 18-20 g/m. Cyclohexylammonium chromate was applied from an aqueous suspension, dicyclohexylammonium chromate and the esters of the chromic acid from alcohol solutions. It was shown that the best protection for steel is obtained with cyclo- and dicyclohexylammonium chromates. Their effect is noticeably higher than that of dischexylammonium nitrite and cyclohexylammonium carbonate. The inhibitors mentioned, especially cyclohexylammonium chromate, have also good protective properties with regard to non-ferrous metals. Experiments with samples made from D-16 Duraluminum and oxidized magnesium alloy showed good protective properties of cyclo- and dicyclohexylammonium chromates with regard to magnesium alloys. The potential of steel, brass, nickel and zinc samples in tap water containing chromates of cyclo- and dicyclohexylammonium was shifted to the side of positive values. The "slit effect", i.e., the intensification of corrosion in narrow gaps is considerable for dicyclohexylammonium chromate.

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S/080/60/033/007/014/020 A003/A001

Amine Chromates and Esters of the Chromic Acid as Inhibitors of Atmospheric Corrosion

It can be suppressed by adding phenyl and butyl benzoates to the inhibitor. There are 3 graphs and 7 references: 2 Soviet, 2 English, 2 German and 1 Czechoslovakian.

SUBMITTED: June 1, 1959

Card 3/3

25072 S/080/60/033/010/026/029 D216/D306

188310

AUTHORS: Gintsberg, S.A., and Shreyder, A.V.

TITLE:

The use of certain amino salts of inorganic acids as inhibitors of the atmospheric corrosion of metals

PERIODICAL: Zhurnal prikladnoy khimii, v. 33, no. 10, 1960,

2366 - 2368

TEXT: Owing to the great diversity of their composition and service conditions, many metallic articles are not given any adequate protection by common inhibitors. Therefore, an investigation of the protective action of packing paper impregnated with aminosalts and certain inorganic acids was carried out. The amine cations were selected to include a nitrogen-containing group, so as to facilitate irreversible sorption onto the surface of the protective metal. The anions of the salts had to provide either a passivating or a film-forming action of the inhibitor. Molybdates and wolframates were used as representatives of the former, and phosphates and

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<sup>2</sup>5072 S/080/60/033/010/026/029 D216/D306

The use of certain amino ...

borates of the latter. Corrosion tests were carried out in a cabinet, using periodic heating and cooling. The temperature was maintained at 40° for 1 hour, reduced to 20° for 2 hours, and was then raised again, etc. The relative humidity was maintained at 92-94 % at all temperatures by means of glycerine solutions. 0.01 mg/1 SO, gas was introduced into the cabinet daily. The effectiveness of the protective action was estimated for steel according to the proportion of the surface having suffered corrosion, and for non-ferrous metals, by a specially designed 10-point scale. In this scale, Class 1 corresponds to the presence on the metal surface of slight tarnishes which wash off easily, or of deposition of inhibitors, Class 2 - appearance of tarnishes which cannot be washed off, Class 3 - single corrosion pits, Class 4 - pitting corrosion, Class 5 - pits with corrosion products, Class 6 - separate stains on the external surface, Class 7 - stains on both surfaces, Classes 8 - 10 - intense corrosion with formation of considerable quantities of corrosion products, the paper sticking to such a surface. Packing paper was saturated with aqueous solutions of inhibitor in Card 2/3

25072 S/080/60/033/010/026/029 D216/D306

The use of certain amino ...

such a way as to ensure the presence of  $15-20~\rm g/m^2$  of inhibitor in the packing paper. Salt losses after long exposure under conditions of small temperature variations  $(20\pm2^{\circ})$  and humidity  $(50\pm5\%)$  were studied parallel with the corrosion tests. These losses were due to volatilization. The changes in relative volatilization with time are shown. The authors conclude that among the tested salts only monc- and tri-ethynolamine borates can be regarded as possible inhibitors of atmospheric corrosion for steel articles containing, apart from uncoated components, nickel and zinc plated components or components made of zinc and nickel-base alloys. There are 2 figures and 4 references: 3 Soviet-bloc and 1 non-Soviet-bloc. The reference to the English-language publication reads as follows: Hackerman and A.C. Macrides, Ind. Eng. Ch., 46, 3, 523-527, 1954.

SUBMITTED: November 12, 1959

Card 3/3

85447

S/080/60/033/011/006/014 A003/A001

18.8300 exclude 2408

Shreyder, A. V., Gintsberg, S. A.

TITLE: On the Slit Effect in the Inhibition of Atmospheric Corrosion

PERIODICAL: Zhurnal prikladnoy khimii, 1960, Vol. 33, No. 11, pp. 2541-2547

TEXT: The slit effect of corrosion was determined on samples (0.1 mm thick) of  $y_{12}$  (U12) steel of 22 x 15 mm. Two of these samples were packed together and the difference of corrosion on their outside and inside surfaces was investigated. The samples were kept in corrosion chambers with continuously changing temperature (20°C for 2 hours and 40°C for 1 hour), a humidity of 94-96% and a content of 0.1 mg/l of sulfur dioxide in the air. The index of the slit effect was determined by the formula  $A = \frac{I}{I+0}$ . 100%, where I is the area affected by corrosion on the

inner surfaces of the samples, 0 is the outer surface affected by corrosion. [Abstractor's note: I (inner) is a translation of the Russian V (vnutrennyy) and O (outer) a translation of N (naruzhnyy)]. It was shown that the slit effect increases with the capillary condensation in the gap. If thin samples (0.1 mm) are packed with thick samples (0.4 mm) the slit effect decreases from 81.7 - 96.4%

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On the Slit Effect in the Inhibition of Atmospheric Corrosion

to 41.2 - 76.1% when using ammonium benzoate as inhibitor. Among the 32 inhibitors tested, the slit effect is manifested when compounds are used like ammonium benzoate, dicyclohexylammonium chromate. Stimulators of corrosion (diphenylguanidine) and indifferent compounds (diphenylguanidine benzoate) can also give rise to slit effect. The use of the following substances, which are non-volatile and stimulators of corrosion, is not accompanied by the slit effect: monoethanolamine tungstate, triethanolamine tungstate, the ammonium salts of synthetic fatty acids, the sodium salt of alkylsulfoacid, the sodium salt of aliphatic aminoacid. Many inhibitors stop corrosion only in the presence of oxygen. The reduced aeration in the slit decreases the effect of passivators. A special inhibitor was tested which contained an "antislit" admixture. For this purpose 7.5 to 50.0% (based on the inhibitor weight) casein and albumin glues, phenylbenzoate, phenyloleate, butylbenzoate and the sodium salt of a mixture of monoand diesters of orthophosphoric acid was added to chromates of cyclohexylammonium and dicyclohexylammonium, ammonium benzoate and diphenyl guanidine and to a mixture of urotropine with sodium n'Itrite. The slit effect was abolished and the protective properties were increased somewhat by adding (in the ratio 1: 2) butyl-

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85447

S/080/60/033/011/006/014 A003/A001

On the Slit Effect in the Inhibition of Atmospheric Corrostion

and phenylbenzoate to chromates of cyclo- and dicyclohexylammonium and to ammonium benzoate. There are 2 figures, 3 tables and 13 references: 11 Soviet, 2 English.

SUBMITTED: March 7, 1960

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AKOL'ZIN, P.A., doktor tekhnicheskikh nauk; SHREYDER, A.V., dotsent, kand. tekhn.nauk

"Theory of the corrosion and protection of metals" by N.D. Tomashov. Reviewed by P.A. Akol'zin. Zav. lab. 27 no. 4:503 '61.

(Corrosion and anticorrosives) (Tomashov, N.D.)

#### "APPROVED FOR RELEASE: 07/13/2001

CIA-RDP86-00513R001550010004-5

S/080/61/034/008/011/018 D204/D305

AUTHOR:

Shreyder, A.V.

TITLE:

On evaluating the effectiveness of anodic oxidation of aluminum alloys by the coefficient of cover-

age

PERIODICAL:

Zhurnal prikladnoy khimii, v. 34, no. 8, 1961,

1779-1786

TE(T: The peculiarities of anodic oxidation of metals make it impossible for characteristics such as current efficiency, energy efficiency etc. to be used for evaluating the effectiveness of this process. In order to overcome this difficulty, a new concept, the process coefficient" (Cc) was coined by R.B. Mason and C. Slunder "coverage coefficient" (Cc) was coined by R.B. Mason and P.E. (Ref. 2: INd. Eng. Ch. 39, 1, 2, 1947) and R.B. Mason and P.E. Fowle (Ref. 3: J. Electrochem. Boc., 101, 2, 53-59, 1954). In order to assess the value of Cc. the sensitivity with which this factor reacts to any change in the parameters of the anodizing process was determined, and efforts made to find the extent to which changes

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S/080/61/034/008/011/018 D204/D305

On evaluating the effectiveness....

in C<sub>c</sub> can be explained logically on the basis of the known mechanism of the process of anodic oxidation of aluminum and its alloys. The alloys AMg (2.4% Mg, 0.3% Mn), D-1, (4.5% Cu, 0.8% Mg, 0.8% Mn) and AK-6 (2.2% Cu, 0.6% Mg, 0.6% Mn, 1.0% Si) were used in this investigation. Anodizing was carried out in 3 electrolytes: 20% H<sub>2</sub>DO<sub>4</sub>, 3% CrO<sub>3</sub> and 10% CrO<sub>3</sub>, with various times and working temperatures. The oxide film was removed in a solution containing 20 g/l CrO<sub>3</sub> + 35 ml/l H<sub>3</sub>PO<sub>4</sub> (specific gravity 1.6) at 90°, during a 10-minute immersion. The at ack of AMg by the stripping solution was negligible, and as regards the alloys D-1 and AK-6 it was allowed for in a correction. The following relationships were studied for all 3 alloys in the above electrolyte: C<sub>c</sub> against time of anodizing, temperature and weight of metal oxidized during anodizing. The influence of the working voltage used in anodizing in a 3% CrO<sub>3</sub> solution of the change of C<sub>c</sub> during film formation on the AK-6 alloy was studied, and the relationships between C<sub>c</sub>, weight of film formed, and weight of oxidized metal against time of anodizing for the D-1 alloy in the same solution were also investigated. It was found

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On evaluating the effectiveness...

S/080/61/034/008/011/018 D204/D305

that the value of  $G_C$  provides a clear indication of the effectiveness of the anodizing process only in a limited range of anodizing conditions (e.g. in a 20% H<sub>2</sub>SO<sub>4</sub> electrolyte at temperatures from k.T. upwards). A change in the value of  $G_C$  need not correspond to any change in the quality of the films or the practical effectiveness of the film formation process, the latter being dependent on the parameters of the process as well as the nature of the aluminum alloy being anodically oxidized. There are 5 figures, 1 table and 5 references: 2 Soviet-bloc and 3 non-Soviet-bloc. The references to the English-language publications read as follows: R.P. Mason, G. Slunder, Ind. Eng. Ch., 39. 1, 2 (1947); R.P. Mason, P.E. Fovle, J. Electrochem. Soc., 101. 2, 53-59 (1954); J.M. Kape, Netal Ind. 91. 4012 (1957)

SUBMITTED:

August 29, 1960

Card 3/3

5/080/62/035/002/021/022 D204/D302

18.1151 AUTHORS:

Shreyder, A. V. and Degtyareva, G. L.

TITLE:

Relationship between heat resistance and velocity constants of the exidation reactions of chrome and

Zhurnal prikladnoy khimii, v. 35, no. 2, 1962, 455-458 chrome-nickel steels

PERIODICAL:

TEXT: Oxidation of 15 steels (compositions tabulated) was studied at 900 + 5°C, over 100, 200, 300, 400, 500, 700 and 1000 hours in at 900 + 5°C, over 100, 200, 300, 400, 500, the weight-gain method.

The oxidized layers were stripped off electrolytically in a molt. The oxidized layers were stripped off electrolytically, in a melt of 60% NaOH/40% Na<sub>2</sub>CO<sub>3</sub>, at 350 - 400°C, using current densities of 40 - 50 A/dm<sup>2</sup>, over 5 - 15 minutes. The results are shown graphically. It was found that steels 1×18 H9T, ×23 H13, ×25 T, ×18 H14 C2 A, ×18 H14 C2 F3 A and ×18 H14 C2 F2 A (1Kh18N9T, Kh25N13, Kh25T, Kh18N11S2A, Kh18N11S2G3A and Kh18N11S2G2A) oxidized parabolically whilst steels Kh18N11S2G3A and Kh18N11S2G2A) Oxidized parabolically whilst Steels ×23H11, ×25H20C2, ×25H05, ×20H14C2, ×25H16F1AP, ×25H16F1C2AP,

Card 1/2

GAVRILYUK, Anatoliy Mefod'yevich; SHOBIK, L.Ye., inzh., ved. red.; SHREYDER, A.V., kand. tekhn.nauk, red.; PONOMAREV, V.A., tekhn. red.

[Anticorrosion coatings and materials for tropical climate conditions] Antikorrosionnye pokrytiia i materialy dlia uslovii tropicheskogo klimata. Moskva, Filial Vses. in-ta nauchn. i tekhn. informatsii, 1958. 7 p. (Peredovoi nauchno-tekhnicheskii i proizvodstvennyi opyt. Tema 13.

No.M-58-178/20)

(Corrosion-resistant materials-Climatic factors)

(Protective coating-Climatic factors)

TITOV, Vasiliy Alekseyevich, kand.tekhn. nauk; YAKUBENKO, Arnol'd Romanovich, inzh.; SHOBIK, L.Ye., inzh., ved. red.; SHREYDER, A.V., kand. tekhn. nauk, red.; SOROKINA, T.M., tekhn. red.

[Effectiveness of steel protection against corrosion by various methods of oxidation]Effektivmoet' zashchity stali ot korrozii razlichnymi metodami oksidirovaniia. Moskva, Filial Vses. in-ta nauchn. i tekhn. informatsii, 1958. 14 p. (Peredovdi nauchno-tekhnicheskii i proizvodstvennyi opyt. Tema 13. No.M-58-108/11) (MIRA 16:3)

(Steel--Corrosion) (Metallic films)

GOL'DSHTEYN, Mark Yefimovich; SHOBIK, L.Ye., inzh., ved. red.; SHREYDER, A.V., kand. tekhn. nauk, red.; SMIRNOV, B.M., tekhn. red.

[Electrodeposition of nickel-phosphorus alloys] Elektroliticheskoe osazhdenie splava nikel - fosfor. Moskva, Filial Vses. in-ta nauchn. i tekhn. informatsii, 1958. 15 p. (Peredovoi nauchno-tekhnicheskii i proizvodstvennyi opyt. Tema 13. No.M-58-132/14) (MIRA 16:3) (Nickel-phosphorus alloys) (Electroplating)

BOGORAD, Lev Yakovlevich; GUTKIN, Ben'yamin Girshevich; SHOBIK, L.Ye., inzh., ved. red.; SHREYDER, A.W., kand. tekhn.nauk, red.; PAUTIN, N.V., inzh., red.; SOROKINA, T.M., tekhn. red.

[Wear resistant chromizing with periodic current reversal]Iznosostoikoe khromirovanie pri periodicheskom izmenenii napravleniia toka. Moskva, Filial Vses. in-ta nauchn. i tekhn. informatsii, 1958. 23 p. (Peredovoi nauchno-tekhnicheskii i
proizvodstvennyi opyt. Tema 13. No.M-58-245/25) (MIRA 16:3)
(Chromium plating)

AROBELIDZE, Aleksandr Konstantinovich; SHOBIK, L.Ye., inzh., ved. red.; SHREYDER, A.V., kand. tekhn. mauk, red.; SOROKINA, T.M., tekhn. red.

[Improved technology of porous chromium plating]Usovershenstvovanie tekhnologii poristogo khromirovaniia. Moskva, Filial Vses.in-ta nauchn. i tekhn. informatsii, 1958. 19 p. (Peredovoi nauchno-tekhnicheskii i i proizvodstvennyi opyt. Tema 13.

No.M-58-244/24) (Chromium plating)

SHOBIK, L.Ye., inzh., ved. red.; KCNAREV, M.I., kand. khim. nauk, red.; SHREYDER, A.V., kand. tekhn. nauk, red.; PONOMAREV, V.A., tekhn. red.; SOROKINA, T.M., tekhn. red.

[Protection of metals from corrosion; wear-resistant, finishing, and decorative coatings] Zashchita metallov ot korrozii, iznosostoikie, otdelochnye i dekoratiwnye pokrytiia. Moskva, Filial Vses. in-ta nauchn.i tekhn. informatsii. Nos.1-8. 1958. (Peredovoi nauchno-tekhnicheskii i proizvodstvennyi opyt. Tema 13. Nos.M-58-19/2, M-58-60/5, M-58-95/8, M-58-96/9, M-58-100/10, M-58-169/19, M-58-257/26, M-582/27) (MIRA 16:3)

(Corrosion and anticorrosives) (Electroplating)

KARRA, Valentin Yakovlevich; MININ, Aleksandr Savel'yevich; SHOBIK, L.Ye., inzh., ved. red.; SHREYDER, A,V., kand.tekhn.nawk, red.; PONOMAREV, V.A., tekhn. red.

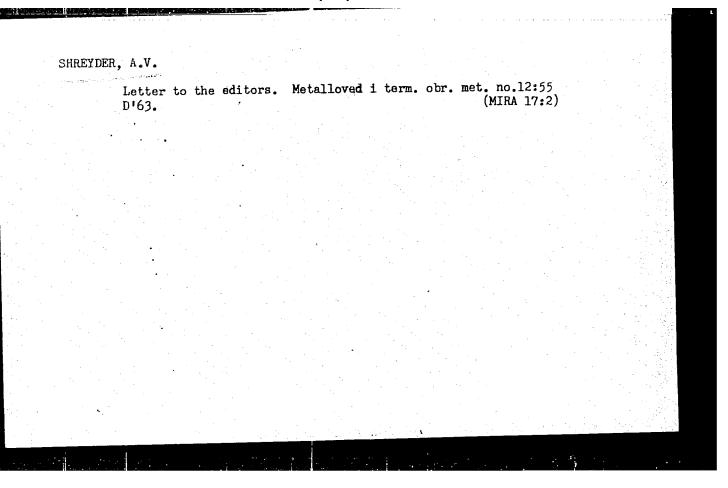
[Performance of chromium plating steel baths with passivation linings and cathodic protection. Molybdenum coating of aluminum and its alloys]Rabota stal nykh khromovykh vann s primeneniem passivirovaniia i katodnoi zashchity. Molibdenirovanie aliuminiia i ego splavov. Moskva, Filial Vses. inta nauchn.i tekhn.informatsii, 1958. 10 p. (Peredovoi nauchnotekhnicheskii i proizvodstvennyi opyt. Tema 13. No.M-58-265/28) (MIRA 16:3)

(Chromium plating-Equipment and supplies)
(Protective coatings) (Aluminum)

SHREYDER, Aleksandr Viktorovich, kand. tekhn.nauk; DEGTYAREVA, Galina L'vovna; SHLUGER, M.A., red.; NAUMOV, I.D., nauchnyy red.; VASIL'YEVA, F.A., ved. red.; LADONINA, L.V., tekhn. red.

[Corrosion resistance of aluminum and the use of aluminum in various branches of industry; review of practices in foreign countries] Korrozionnaia stoikost' aliuminia i ego primenenie v razlichnykh otrosliakh promyshlennosti; obzor sarubezhnoi tekhniki. Moskva, Gos.nauchno-issl. in-t nauchn. i tekhn. informatsii, 1962. 62 p. (MIRA 16:4)

(Aluminum--Corrosion)



D'YAKOV, V.G.; LEVIN, I.A.; SHREYDER, A.V.

Aluminum, titanium, and OKH21N5T and KH21N6M2T low-nickel steels as materials for the equipment of petroleum refineries and petrochemical plants, Mash, i neft, obor, no.4:27-33 63. (MIRA 17:8)

1. Gosudarstvennyy nauchno-issledovatel'skiy i proyektnyy institut neftyanogo mashinostroyeniya.

ACCESSION NR: AT4043068 S/0000/64/000/000/0035/0047

AUTHOR: Shreyder, A. V.

TITLE: The activation energy and mechanism of anodic oxidation of Al alloys

SOURCE: Mezhvuzovskaya konferentsiya po anodnoy zashchite metallov ot korrozii. 1st, Kazan, 1961. Anodnaya zashchita metallov (Anodic protection of metals); doklady\* konferentsii. Moscow, Izd-vo Mashinostroyeniye, 1964, 35-47

TOPIC TAGS: aluminum alloy, nodized aluminum alloy, anodic exidation, activation energy, Arrhenius graph method, alloy h 3, alloy D1, alloy AK6, sulfate electrolyte anodizing, chromate electrolyte anodizing, a die film formation, aluminum exidation

ABSTRACT: The author sought to cla fy the mechanism of formation of an anodic oxide film by analyzing the activation energies of film formation and aluminum oxidation. He introduces the concept of elementary stages (I - VI) of anodic oxidizing of Al and its alloys, describing these and parallel reactions occurring at each stage in tabular form. Activation energies were calculated from Arrhenius graphs for samples of alloys AMg, D1 and AK6 (compositions given, latter two hardened and artificially aged, former unhardened), anodized in three electrolytes (20% H<sub>2</sub>SO<sub>4</sub>, 10% CrO<sub>3</sub>, or 3% CrO<sub>3</sub>; 15—120 min., 25-55C).

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ACCESSION NR: AT4043068

Weight differences between the oxidized sample and a sample with the oxide film removed (10 min., 90C, 20 g/1 CrO<sub>3</sub> and 35 ml/1 H<sub>3</sub>PO<sub>4</sub> -- sp. gr. 1.6) served as the quantitative criterion of film formation, while loss of aluminum was the criterion of the aluminum oxidation process. The employed method produced apparent energy values (tabulated) which differed significantly from true activation energies by values for heats of adsorption hydration, etc. It was not possible to determine with this method whether direct oxidation of Al by oxygen or the cross diffusion of Al3+ and O2- ions in the oxide film is the controlling stage of the process. "The author expresses his gratitude to V. V. Skorcheletti for his evaluation of this study". Orig. art. has: 3 tables and 27 graphs.

ASSOCIATION: None

SUBMITTED: 13Mar64

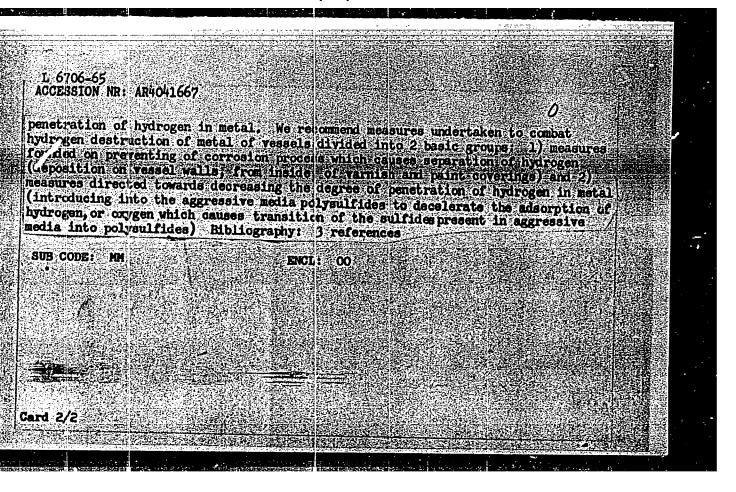
NO REF SOV: 006

ENCL: 00

OTHER: 001

SUB CODE: MM

6706-65 BWT(m)/BWP(q)/EWP(b); AF	π <sub>3</sub> (τ <sub>D</sub> )/ASD(m)=3 JD
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CESSION NR: AR4041667 DURCE: Ref. zh. Khimicheekoye 1 kho os. 5:47:10	ldil noye mahinostroyeniye. Otd. vy'p.
UTHOR: Shreyder, A. V.; Shparber, I	, Si; Varfolomeyev, V. V.
INTE: Stratification of metal of ve	8.5el Vell8
ITED SOURCE: Bezopasnost's truda pro	om-sti, no. 1, 1964, 1/219
	ssel wall, hydrogen penetration, hydrogen
PRANSLATION: In the last 2 - 3 year	s in a number of enterprises of oil refining technological apparatures working with media technological apparatures from 30 to 50°C; and moisture at temperatures from 30 to 50°C;
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	here were repeatedly revealed s of bubbles and a large quantity of <u>cracks</u> . to be penetration of hydrogen in steel of we lamage of metal and conditions promoting the
considered the process of hymogen	
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D'YAKOV, V.G., kand. tekhn. nauk; SHREYDER, A.V., kand. tekhn. nauk; CHEREPAKHOVA, G.L., inzn.

Using aluminum alloys for petroleum heat-exchanging equipment. Khim. i neft. mashinostr. no.3:31-33 S '64. (MIRA 17:12)

L.2L681-65 EWT(m)/EWA(d)/EPR/EWP(t)/EWP(b) Pa-L IJP(c) ACCESSION NR: AR5000966 \$/0282/64/000/010/0002/0002 SOURCE: Ref. zh. Khimicheskoy / kholodil noye máshinostroyeniye. Otd. Abs. 10.47.18 AUTHOR: Shreyder, A. V.; Degtyareva, C. L., Sukhacheva, S. V. TITIM: Ocidation of magnalium by water at high pressures and temperatures 10 CITED SOUNCE: Tr. Gos. n.-i. i proyektn; in-t neft; mashinostr,, vyp. 2, 1964, 67-72 TOPIC TACK: magnalium piping, anticorrosion oxidation, condensation piping, water supply piping, distilled water oxidation; protective film index; piping oxidation technique, pipeline corrosion, aluminum alloy corrosion TRANSLATION: Piping for water supply and condensation cooling equipment used in many manufacturing processes of the oil refining, petrochemical and other branches of industry is made of magnalium in view of the alloy's high corrosion stability and technological qualities. Magnalium piping is nonetheless subject to some corrosion after a given period of exposure and the attack is lintensified when the recirculating cooling water contains impurities. The protection of the Card 1/2

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ACCESSION NR: AR5000966

Internal surfaces of such piping by electrochemical oxidation is costly and technically complex. Hence, the possibility of depositing protective films on Al and its alloys by treating them in water at high pressure and temperature is of interest. Tests served to establish that distilled water oxidation can be employed to obtain protective films on magnalium. The protective quality index of such films, evaluated by spot test methods, was JOX lower than the index of films deposited by standard anodic oxidation. Films with peak protective qualities can be deposited on magnalium in distilled water by exposure for S hrs. at 1000, 2 hrs. at 1500 or 1 hr. at 2000. Filling by boiling for 100 min, in a JX solution of water-glass improves by 50 - 1007, the protective quality indices of films deposited by exposures of not less than 2 hrs. at 1500 or 1 hr. at 2000. The thickness of the forming oxide film can be increased 50 - 1007, by adding triethanolamine to the water, but the corresion inhibiting qualities of the film deteriorate at the same times; Bibl. with 6 cities.

SUB CODE: NH, FP EICL: 00

L 33524-65 ENG(1)/EPA(s)-2/ENP(e)/ENT(n)/EPR(c)/EPE(n)-2/ENA(d)/EPR/EPA(w)-2/ ENP(t)/EPA(bb)-:!/EWP(b) Pr-4/Ps-4/Pt-10/Pu-4/Pab-10 IJP(c) WW/MJW/JD/WB/WH ACCESSION NR: AB5005705 S/0276/64/000/010/B081/B081 ACCESSION NR: AR5005705 SOURCE: Ref. zh. Tekhnol mashinostri Sv. (., Abs. 10B549 AUTHOR: Shreyder, A.V.; Degtyareva, G.I. TITLE: Corrosion of magnalium at high temperatures and the protective effect of an anodic oxide coating CITED SOURCE; Tr. Gos. n. 1 proyekin. in t neft; mashinostr., vyp. 2, 1964, 83-90 TOPIC TAGS: magnalium, high temperature corrosion, anodic oxidation, oxide protectiv property TRANSLATION: The results of corrosion resistance tests on anodized samples of magnalium (alloy AMg5 with 4.8% Mg) are presented. It was shown that high temperature corrosion of magnalium at represents a process attenuating in time up to 450C inclusive. When heated in air, anodic oxide coatings are subject to dehydration and cracking as a result of successively occurring structural conversions; i.e. hydrargillite (bayerite) to boehmite, to leached boehmite, to amorphous alumina) to crystalline Al<sub>2</sub>O<sub>3</sub>. The ability of an anodic oxide coating to project against atmospheric corrosion at normal temperatures deteriorates increasingly as temperature and exposure period are Card 1/2

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ACCESSION NR: AR5005705		
ingregated when anodized magnatium is heater	id in air. Eissures resulting from dehydra-	
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tion and cracking of anodic oxide tilms are place when the material is heated in air. A protective properties against high temperatu	ire oxidation up to the melting point for	
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SUB CODE: MM ENCL: 00		
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DIYAKOV, V.G., kand.tekhn.nauk; SHREYDER, A.V., kand.tekhn.nauk; ZAKHAROCHKIN, L.D., inzh.

Basic trends in controlling the corrosion of petroleum refinery equipment. Khim.i neft. mashinostr. no.8:4-5 Ag '65. (MIRA 18:12)

SHREYDER, A.V., kand.tekhn.nauk; SHPARBER, I.S., inzh.; ZHUK, N.P., doktor tekhn.nauk

Corrosive exfoliation of metals of petroleum-refinery low temperature equipment. Khim. i neft. mashinostr. no.9:28-32 (MIRA 18:10)

CHEREFAKLOVA, G.L., KIINOV, J.Ya.; SHREYDNR, A.V.

Corrosion resistance of aluminum alloys in the condenser refrigerating equipment of petrochemical industries.

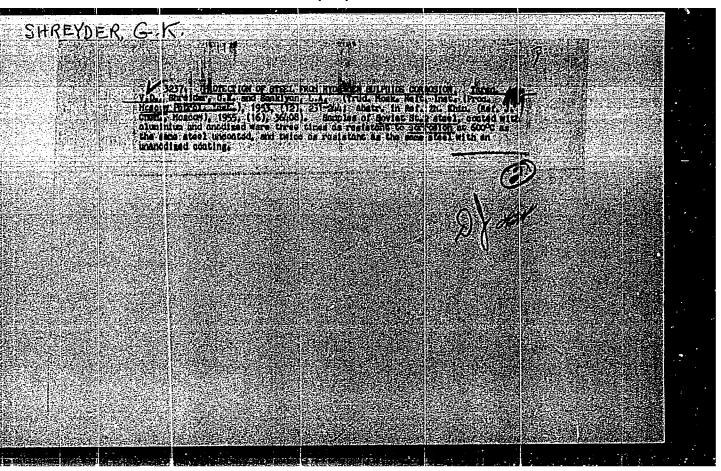
Trudy MiKHM 28:117-126 164.

(MIR4 19:1)

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ACC NR: AP6028095 (N) SOURCE CODE: UR/0314/66/000/006/0023/0026  UTHOR: Cherepakhova, G. L. (Engineer); Shreyder, A. V. (Candidate of technical \$26  ciences); Klinov, I. Ya. (Doctor of technical sciences)		
UTHOR: Cherepakhova, G. L. (Engineer); Threyder, A. V. (Candidate of technical \$\times 9\$ ciences); Klinov, I. Ya. (Doctor of technical sciences)  RG: none  RG: none  RG: none  RG: Effect of the composition of the cooling water on the corrosion resistance of the alloy under the working conditions of condensers in oil refining plants  RG: Mg alloy under the working conditions of condensers in oil refining plants  RG: Mimicheskoye i neftyanoye mashinostroyeniye, no. 6, 1966, 23-26  ROPIC TAGS: corrosion resistance, magnesium containing alloy, manganese containing alloy  ABSTRACT: For the purposes of the tests a synthetic fresh water was prepared, with the following composition: 116 mg/liter NaCl; 49 mg/liter Na2S; 2740 mg/liter Na2Si, 2740 mg/liter Na2Sou, 10 H2O; 10 mg/liter Fe <sub>2</sub> (SO <sub>2</sub> ) 29H <sub>2</sub> O; 266 mg/liter MgSO <sub>4</sub> 7H <sub>2</sub> O; 516 mg/liter Na2SO <sub>4</sub> 2H <sub>2</sub> O; 376 mg/liter NaHCO <sub>3</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 CaSO <sub>4</sub> 2H <sub>2</sub> O; 376 mg/liter NaHCO <sub>3</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 caso, 2H <sub>2</sub> O <sub>4</sub> 2H <sub>2</sub> O; 376 mg/liter NaHCO <sub>3</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 caso, 2H <sub>2</sub> O <sub>4</sub> 2H <sub>2</sub> O; 376 mg/liter NaHCO <sub>3</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 caso, 2H <sub>2</sub> O <sub>4</sub> 2H <sub>2</sub> O; 376 mg/liter NaHCO <sub>3</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 caso and 2H <sub>2</sub> O <sub>4</sub> 2H <sub>2</sub> O; 376 mg/liter NaHCO <sub>3</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 caso and 2H <sub>2</sub> O <sub>4</sub> 2H <sub>2</sub> O; 376 mg/liter NaHCO <sub>3</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 caso and 2H <sub>2</sub> O <sub>4</sub> 2H <sub>2</sub> O; 376 mg/liter NaHCO <sub>3</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 caso and 2H <sub>2</sub> O <sub>4</sub> 2H <sub>2</sub> O <sub>4</sub> 2H <sub>2</sub> O <sub>4</sub> 3H <sub>2</sub> O <sub>5</sub> 3H <sub>2</sub> O <sub>5</sub> 3H <sub>2</sub> O <sub>5</sub>	L 06084-67 EWT(m)/EWP(t)/ETI/EWP(k) IJ	
RG: none  RG: no	ACC NR: AP6028095 (N)	
PITIE: Effect of the composition of the cooling water on the corrosion resistance of Mg Alloy under the working conditions of condensers in oil refining plants  Nounce: Khimicheskoye i neftyanoye mashinostroyeniye, no. 6, 1966, 23-26  TOPIC TAGS: corrosion resistance, magnesium containing alloy, manganese containing alloy  ABSTRACT: For the purposes of the tests a synthetic fresh water was prepared, with following composition: 116 mg/liter NaCl; 49 mg/liter Na <sub>2</sub> S; 2740 mg/liter the following composition: 116 mg/liter NaCl; 49 mg/liter MgSO <sub>4</sub> *7H <sub>2</sub> O; 516 mg/liter Na <sub>2</sub> SO <sub>4</sub> *10 H <sub>2</sub> O; 10 mg/liter Fe <sub>2</sub> (SO <sub>4</sub> ) *9H <sub>2</sub> O; 266 mg/liter MgSO <sub>4</sub> *7H <sub>2</sub> O; 516 mg/liter Na <sub>2</sub> SO <sub>4</sub> *10 H <sub>2</sub> O; 336 mg/liter NaHCO <sub>2</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 CaSO <sub>4</sub> *2H <sub>2</sub> O; 336 mg/liter NaHCO <sub>2</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 CaSO <sub>4</sub> *2H <sub>2</sub> O; 336 mg/liter NaHCO <sub>2</sub> . The pit was 6.5 in chloride solutions, 6.7-6.9 in sulfate solutions, 8.1-8.9 mg/liter. The pit was 6.5 in chloride solutions, 6.7-6.9 in sulfate solutions, 8.1-8.9 mg/liter. The pit was 6.5 in chloride solutions tests were carried out on samples of change during the carrosion tests. The corrosion tests were carried out on samples of change during the carrosion tests. The corrosion tests were carried out on samples of change alloy (2.4% Mg/0.4% Mn) at temperatures of 20 and 45°C which corresponds to the AMg alloy (2.4% Mg/0.4% Mn) at temperatures. The duration of the tests was 360 actual operating temperatures of condenser tubes. The duration of the tests was 360	AUTHOR: Cherepakhova, G. L. (Engineer); Shi	reyder, A. V. (Candidate of technical 26
PITIE: Effect of the composition of the cooling water on the corrosion resistance of alloy under the working conditions of condensers in oil refining plants of condensers in oil refining plants.  Mg alloy under the working conditions of condensers in oil refining plants of condensers in oil refining plants.  Mg alloy under the working conditions of condensers in oil refining plants.  Mg alloy under the working conditions of condensers in oil refining plants.  Mg alloy under the working conditions of condensers in oil refining plants.  Mg alloy under the working conditions of condensers in oil refining plants.  Mg alloy under the working conditions of condensers in oil refining plants.  Mg alloy under the working conditions of condensers undersers in oil refining plants.  Mg alloy under the working conditions of condensers undersers undersers of condensers on the condense containing plants.  Mg alloy under the working conditions of condensers of condensers on the condense containing plants.  Mg alloy under the working conditions of condensers of condensers on the corrosion that conditions of the tests undersers of condenser tubes.  Mg alloy under the working conditions of condenser tubes.  Mg alloy under the working conditions of condensers of condensers on condensers on the corrosion that conditions of the tests undersers of condenser tubes.  Mg alloy under the working conditions of the tests undersers of condenser tubes.  Mg alloy under the working plants.  Mg alloy under the working conditions of condensers of condensers on condensers on condensers on condensers undersers of condensers undersers of condensers undersers of condensers undersers on condensers undersers of condensers		
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ABSTRACT: For the purposes of the tests a synthetic fresh water was prepared, with the following composition: 116 mg/liter NaCl; 49 mg/liter Na2S; 2740 mg/liter Na2S04. 10 H20; 10 mg/liter Fe <sub>2</sub> (SO4)3. 9H20; 266 mg/liter MgSO4. 7H20; 516 mg/liter Na2SO4. 2H20; 336 mg/liter NaHCO3. The permissible content of CuCl2 was up to 1 CaSO4. 2H20; 336 mg/liter NaHCO3. The permissible content of CuCl2 was up to 1 mg/liter. The pH was 6.5 in chloride solutions, 6.7-6.9 in sulfate solutions, 8.1-8.9 mg/liter. The pH was 6.5 in chloride solutions. The pH practically did not in bicarbonate solutions, and 8.2-9.3 in sulfide solutions. The pH practically did not change during the corrosion tests. The corrosion tests were carried out on samples of change during the corrosion tests. The corrosion tests were carried out on samples of change alloy (2.44 Mg, 0.44 Mn) at temperatures of 20 and 45°C which corresponds to the AMg alloy (2.44 Mg, 0.44 Mn) at temperatures. The duration of the tests was 360 actual operating temperatures of condenser tubes. The duration of the tests was 360		stroyeniye, no. 6, 1966, 23-26
ABSTRACT: For the purposes of the tests a synthetic fresh water was prepared, with the following composition: 116 mg/liter NaCl; 49 mg/liter Na <sub>2</sub> S; 27 <sup>4</sup> 0 mg/liter Na <sub>2</sub> S0 <sub>4</sub> ·10 H <sub>2</sub> 0; 10 mg/liter Fe <sub>2</sub> (S0 <sub>4</sub> ) <sub>3</sub> ·9H <sub>2</sub> 0; 266 mg/liter MgS0 <sub>4</sub> ·7H <sub>2</sub> 0; 516 mg/liter NaHCO <sub>3</sub> . The permissible content of CuCl <sub>2</sub> was up to 1 CaS0 <sub>4</sub> ·2H <sub>2</sub> 0; 336 mg/liter NaHCO <sub>3</sub> . The permissible content of cuCl <sub>2</sub> was up to 1 mg/liter. The pH was 6.5 in chloride solutions, 6.7-6.9 in sulfate solutions, 8.1-8.9 mg/liter. The pH was 6.5 in chloride solutions. The pH practically did not in bicarbonate solutions, and 8.2-9.3 in sulfide solutions. The pH practically did not change during the corrosion tests. The corrosion tests were carried out on samples of change during the corrosion tests. The corrosion tests were carried out on samples of change alloy (2.44 Mg, 0.44 Mn) at temperatures of 20 and 45°C which corresponds to the AMg alloy (2.44 Mg, 0.44 Mn) at temperatures. The duration of the tests was 360 actual operating temperatures of condenser tubes. The duration of the tests was 360	TOPIC TAGS: corrosion resistance, magnesiu	m containing alloy, manganese containing
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SHREYDER, M. N., Engineer

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"Investigation of Operational Indexes of Flax-Combine LK-7 and of Problems of Flax-Harvesting Technology." Sub 26 Jun 51, Moscow Inst of Mechanization and Electrification of Agriculture imeni V. M. Molotov

Dissertations presented for science and engineering degrees in Moscow during 1951.

SO: Sum. No. 480, 9 May 55

ZUBKOVA, P. P., FAL'KO, O. S., SHREYDER, M. N.

Flax

Decisively introduce progressive techniques into combine flax. Dost. sel'khoz. no. 8, 1952

Monthly List of Russian Accessions. Library of Congress. November 1952. UNCLASSIFIED.

ZUBKOVA, P., SHREYDER, M.

Machine-Tractor Stations

Petroleum economy at the Matveevo-Kurgan MTS. MTS 12 no. 5, 1952.

Monthly List of Russian Accessions, Library of Congress, August, 1952. UNCLASSIFIED.

SHREYDER, M.N., kandidat tekhnicheskikh namk.

Flax head conveyor. Tekst. prom. 15 ne.11:18-19 N 155. (MLRA 9:1)

(Conveying machinery) (Flax)

SHR&TUER, Mikhail Mikolayevich: MIKITINA, V.M., red.; ZUERILINA, Z.P., tokhn.red.

[Mechanization of flax harvesting] Mekhanizatsiis uborki l'na.
Moskva, Gos.izd-vo sel'khoz. lit-ry, 1957. 87 p. (MIRA 11:2)

(Flax--Harvesting)

SHREYDER, M.N., kand.tekhn.nauk

Possibility of the introduction of machinery for the continuous harvesting of flax. Mekh. i elek. sots. sel'khoz. 19 no.6:16-20 (MIRA 14:12)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut l'na. (Flax--Harvesting)

SHREYDER, M.N., kand.tekhn.nauk; FEDYUKOV, M.F., kand.tekhn.nauk; VLASOVA, M.N., inzh.

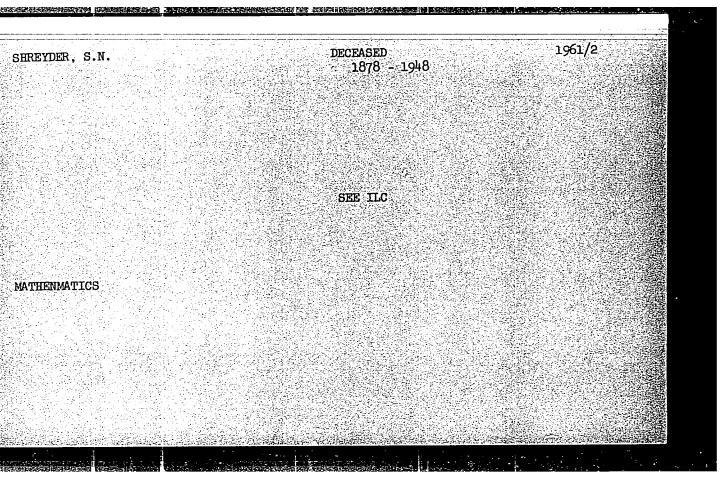
Testing of the ML-2,8 flax thresher. Trakt. i sel'khozmash.
32 no.5:18-20 My '62. (MIRA 15:5)

(Flax processing machinery)

SHREYDER, N. D.

Shreyder, N. D. - "The problem on psychic disturbances in hypertension," Trudy Tsentr. in-ta psikhiatrii, Vol. IV, 1949, p. 135-45

SO: U-4934, 29 Oct 53, (Letopis 'Zhurnal 'nykh Statey, No. 16,1949).



ANTONOV, V.I., kand.tekhn.nauk; SHREYDER, V.A., inzh.

Use of plastic drainage pipes. Gidr. i mel. 13 no.8:29-37
(MIRA 14:8)
Ag \*61.

1. Meshcherskaya zonal\*naya opytno-meliorativnaya stantsiya.
(Drainage) (Pipe, Plastic)

SHREYDER, V.A., kand. tekhn. nauk

Filters for drain pipes. Gidr. i mel. 17 no.11:50-55 N '65. (MIRA 18:11)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut gidro-tekhniki i melioratsii im. Kostyakova.